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1 Introduction

Viscosity is of paramount importance to lubrication engineers, rheologists, chemical engineers, and many more besides. This report describes the background, development, operation and testing of a portable automatic instrument for the measurement of bulk viscosity.

The requirement for such an instrument arose during oxidation studies of new synthetic flourosilicone lubricants, which were carried out by bubbling oxygen through a 20 cm3 quantity at a temperature of 250C. These lubricants have some advantages over conventional hydrocarbon oils: for example they are better suited to harsh conditions such as the extraterrestrial environment. However their high temperature stability is inferior and the oxidation studies were aimed at developing additives to improve performance in this respect.

The condition of the lubricant was monitored by taking hourly samples and measuring the viscosity using a Ferranti-Shirley cone-on-plate viscometer. As the oxidation progressed over several hours or sometimes days, the measured viscosity increased, finally resulting in the formation of a stiff gel. Unfortunately lack of regular data, for example during the night, often resulted in considerable uncertainty regarding the course of the experiment. An automatic viscometer was thus almost essential, particularly for the longer tests. No such instrument was found to be available commercially and so a suitable device was designed and built.

Briefly, this original mechanism stirred the fluid using a glass rod, indirectly driven via a conventional tension spring by a small motor. The extension of the spring was kept constant by means of an electrical contact. Brushes made connection to a simple electronic control circuit which increased the speed while the contact was broken, and decreased it while closed. Thus the rotation rate oscillated around a certain mean value, which was proportional to the viscosity. (See further details on the theory in section 2.) A timer switched the device on at regular intervals for a few seconds, and an output voltage was produced indicating motor speed. This could be plotted on a chart recorder, to obtain a direct graph of relative viscosity against time.

The viscometer just described satisfied the requirement although the accuracy of the measurements was poor. Several possible improvements to the mechanism were foreseen, and in particular the rough nature of the control electronics was an obvious area for further development. In view of this the current project aimed to develop an improved viscometer mechanism and control system. Calibrations and comparisons were also necessary to verity correct operation.

This report considers the theory of fluid viscosity measurement (section 2). The viscometer mechanism, microprocessor control system and operating program are described (section 3). The results of several experiments that were conducted are presented (section 4). Many ideas for further development have occurred during this work, some of which are discussed (section 5). Detailed circuit schematics, program listing, numerical results and the engineering drawings are shown in full in the appendices.

2: Theory of viscosity measurement

2.1 Types of viscometer

The two main types of viscometer are the tube and rotational instruments [ref. 1], The former observe the rate of flow through tubes due to a known pressure difference. These types are unsuitable for this application, because a suitable viscometer must allow the nest of the experiment to proceed normally in the intervals between measurements, The lubrication fluid is contained in a small lest tube or beaker and therefore any tube-like measurements would be impractical and hard to automate.

The vast majority of rotational viscometers fall into two categories: those where two concentric cylinders rotate relative to one another around a common axis; and those consisting of a cone of large vertical angle (approaching 180 degrees), and plate whose plane is through the apex of the cone. Many variations on this theme are possible, but in all types the test fluid is sheared between the rotating parts. The cone on plate type is again rejected for this application, as it would not be possible to perform oxidation experiments inside the viscosity measurement apparatus.

A concentric cylinder viscometer can easily be formed by regarding a beaker in which the experiments are performed as the outer cylinder, and placing a rotating inner cylinder centrally within it. The suitability and simplicity of this arrangement makes it the ideal choice here. Hence the following theoretical derivations are only concerned with instruments of this type.

2.2 Viscosity

Prior to detailed mathematical consideration, it is necessary to define two variables used in the description of fluid flow: shear stress and shear strain. Stress is measured in units of Pascals (1 Pa $=$ I Nm-2). Consider a point P in a body, surrounded by a plane of area A. The material above, below and to the sides of P exert a resultant force F on the element. As the area is varied the force changes, and the ratio F/A approaches a limit as A tends to zero, known as the traction across the area. This traction has a perpendicular component, the 'normal stress', and a parallel component the 'shear stress' s. Shear strain y is defined as the relative displacement of two layers in the fluid, divided by their separation.

A Newtonian fluid is one in which the ratio of shear stress to the rate of shear strain is constant [ref. l].This parameter is the viscosity n. That is,

 $n = s / v$.

The unit of viscosity is the poise. Kinematic viscosity v is often used and is defined as $v=n/p$,

where p is the density of the fluid. The unit of kinematic viscosity is the Stokes; lubricants are usually specified, by convention, in terms of their kinematic viscosity in centistokes (cst).

A non-Newtonian fluid is one in which the viscosity is not a constant parameter, it depends in some way on the shear rate. The Newtonian model is accurate over a large range for most low molecular weight fluids, including water and many aqueous solutions, liquid metals, organic compounds, and silicones. Other fluids such as suspensions obey various more complex models. A large number of such models have been proposed, for example the Bingham [ref. 2], power law fluid [ref. 3], and Casson [ref. 1] models. This report is only concerned with the measurement of viscosity for Newtonian fluids, although modifications to allow for Non-Newtonian behaviour would not be difficult (See discussion, Section 5).

2.3 Concentric cylinder viscometer.

The formulae derived apply to the measurement of Newtonian fluids, confined between concentric cylinders of infinite length, and neglecting any inertial effects [ref. 1]. The inner and outer cylinders are of radius R1 and R2 respectively, and rotate with a relative angular velocity O. Considering the fluid between the inner cylinder and a radius r; each particle moves with a constant angular velocity, such that the net torque on the fluid is zero. The torque G per unit length on a cylindrical surface at radius r is

 $G = 2$ pi R1^2 s1

where s1 is the shear stress on the inner cylinder, The shear stress at any radius r is $s = G / 2$ pi r^{^2}

and in particular, at the outer cylinder is s2=G / 2 pi R2^2.

Figure 1: Horizontal section of a concentric cylinder viscometer and deformation of a fluid element.

An expression for the strain rate may be derived using figure 1, which shows sectors of two cylindrical surfaces separated by a small distance dr. In a time dt the radial line AB moves to AB', as opposed to A'C, had the fluid been a rigid body. Now, $BB' = (r + dr)$ (w + dw) dt

and

 $BC = (r + dr)$ w dt so the shear strain is $y = B'C / CA' = (r + dr) dw dt / dr$, which in the limit as dr tends to zero, gives $dy / dt = r dw / dr$ Substituting these results into the Newtonian fluid equation leads to

r dw / dr = G / 2 pi v r^2

Applying the boundary conditions to $w = 0$ at $r = R1$, $w = Q$ at $r = R2$, and integrating gives $O = G (1 / R1² - 1 / R2²) / 4 pi n$

For a Newtonian fluid a graph of angular velocity against torque per unit length will be linear through the origin, and have gradient

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(1 / R1<sup>2</sup> - 1 / R2<sup>2</sup>) / 4 pi n
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This formula will be used to obtain the viscosity. If the instrument is calibrated with a liquid of known viscosity, or used to measure relative viscosity, then all subsequent measurements can be referenced to this and it is not necessary to know R1 or R2 explicitly, provided they remain constant.

2.4 Deviations from the ideal model

2.4.1 End effects

A practical concentric cylinder viscometer must be of finite size, and therefore the top and base of the inner cylinder will also exert a torque. Furthermore, near to the ends, the torque per unit length will be reduced since the velocity gradient is no longer radial. This necessitates complex

corrections to the formula derived above; however, the torque is still proportional to angular velocity. Hence provided calibration is performed, the end effects will not cause error.

2.4.2 Temperature dependence

Viscosity is highly dependent on temperature. The relation is often found to approximate $v = A exp (Ev / kT)$

over a large temperature range, where v is the kinematic viscosity, k Boltzmann's constant, and T the temperature. The constants A and Ev (known as the activation energy for viscous flow) exhibit a large variation between different fluids. This relation was tested, see section 4.2.

The fluid must he kept at a known and constant temperature throughout the measurement. If the concentric cylirider viscometer is used with very viscous fluids at high shear rates, temperature rise due to shear heating can be troublesome. This effect is neglected here, but is considered further in the discussion, section 5.

2.4.3. Departure from circular flow

In concentric cylinder arrangements, fast moving fluids near to the inner cylinder try to move outwards due to the centripetal force. Such a movement is impossible for the liquid as a whole, so local circulation occurs [ref 4]. These 'Taylor vortices' are only formed above a certain rate of rotation, as in figure 2. This secondary flow is still regular but complex, and the relations derived above no longer apply. At still higher speeds the flow becomes turbulent For Newtonian fluids, the 'Reynolds number' is defined as

 $Re = O R (R2 - R2) / v$

where R is the radius of the moving cylinder, and the other variables are as before.

For inner cylinder rotation, Taylor [ref. 5] found that vortices occurred for

 $Re > 41.3$ (R2 / (R2 - R1)) ^ l/2

At a rotation rate of 300 rpm, and with inner and outer cylinders of radius 1 and 2 cm respectively, the

corresponding minimum kinematic viscosity which may measured is 0.005 cst. The current viscometer will not handle such low viscosities.

Figure 2: Secondary flow patterns at high rotation rates, known as Taylor vortices.

3.1 Viscometer Mechanism.

Operation of the viscometer mechanism is now described, see figure 3; Complete engineering drawings are shown in Appendix C. All major parts were machined from Dural, with the exception of the stirrer: the corrosive nature of the lubricants under study necessitates the use of glass for this component. In all experiments the assembly was suspended above the test fluid by a retort stand.

A small DC motor (A) drives the disk (E), the outer edge of which is removed over 180 degrees, as shown in the detail. Disk (F) is also cut in a similar way. Disks (E) and (F) may rotate independently about the same axis, due to the bearings in (E) and lower plate (C). The outer end of spiral hair spring (1) is bolted to (E) , while the inner end slots into part (F) . Therefore the lower disk (F) is indirectly driven by the upper disk (E), via torque spring (I). Connected to (F) by means of a pinned push-fit joint is the chuck (G). Three nylon screws in this component clamp the glass stirring rod (J) securely. The dimensions of the cylindrical, stirring end of (J) restrict the instrument to measurement over a certain range of viscosity. Different ranges can easily be obtained by altering the size of this stirring cylinder. In the following experiments two stirrers were used, one with a cylinder diameter of 2cm and length of 2cm, the other with a cylinder diameter of 1 cm and length 2cm.

An infra-red light beam is emitted by the LED (L), and passes through the mechanism before detection by the photo diode (M). The LED cover (D) ensures that the beam is sufficiently narrow that reflections from parts of the mechanism do not disrupt readings.

The mounting plates (B) and (C) are supported by four corner pillars, (K). Side plates (H) are fitted; these perform the multiple functions of increasing the rigidity of the structure, excluding dirt, and preventing ambient light from corrupting the infra-red beam measurements.

In operation, the motor rotates at a speed up to 300 rpm, determined hy the control electronics (see section 3.2). The stirrer is turned via the spiral spring, which provides a torque proportional to its angular extension. Thus the relative angular displacement between disks (E) and (F) depends directly on the viscosity of the fluid and rotation rate (see section 2.3 theory). As described, parts (E) and (F) are cut away over 180 degrees; this causes the beam to be interrupted once per revolution. Calculation of the mark/space ratio results in the angular displacement, whilst the motor speed may be accurately determined from the period. Figure 4 illustrates the mechanism operation with liquids of different viscosities, and also shows the corresponding expected photo-diode outputs.

Figure 3: The viscometer mechanism.

A serious problem occurred with the spiral spring. Such a component is difficult to obtain commercially, consequently one was wound from a strip of plate brass approximately 30 cm long, 2 mm wide and 0.5 mm thick. Unfortunately the quality of the spring thus produced was unsatisfactory: only about 3 turns were possible and the spiral shape was difficult to maintain. In addition it was impossible to keep the spring planar: the result of this was that when mounted in the mechanism, the spring scraped on disks (E) and (F) (refer to figure 3). Undoubtedly the instrument's measurement accuracy was seriously affected by the additional friction, hysteresis and non-linearity of this component. Nevertheless useful results were obtainable, as described in section 4, proving the principle and justifying future pursuit of a suitable spring.

Figure 4: Operation of the viscometer mechanism. The diagrams on the left show the relative orientations of the rotating parts (E) and (F), those on the right show the type of photodiode outputs that may be expected from these configurations.

3.2 Microprocessor control system.

Microprocessors are used increasingly in scientific instruments to handle control functions which would previously have been carried out by a dedicated electronic analogue control circuit A microprocessor control system outperforms its less complex predecessor in almost all respects. It is programmable, so that modifications or specific application requirements may easily be applied without total redesign. The system may be programmed to make detailed calculations and statistical analysis, and adapted to make corrections for non-linearity in the measurement device;

hence greater accuracy is achieved. Data logging can be accomplished with ease, so that operation is totally automatic. Calibration of the instrument also becomes simple, and results can be displayed in a manner superior to that obtainable from an analogue unit. Such advantages justify the additional complexity and cost of a microprocessor based system. For these reasons a microprocessor control unit was designed to control the viscometer mechanism. Of course, a standard commercial computer such as a PC could have been used. However, the expense and inconvenience of dedicating a powerful computer was felt to be excessive, and a self-contained unit was considered more attractive.

A block diagram of the circuit used is shown in figure 5. Appendix A may be consulted for a full schematic.

Processor Unit:

An 8-bit Z80B microprocessor was chosen to form the heart of the system. This processor was certainly the most powerful of its generation and despite today's proliferation of faster 16 and 32 bit processors, the Z80 still has much to commend it. Literature on the device abounds; and in particular, designing a system around the Z80 is considerably simpler than for a more powerful processor, leading to a lower component count and cost. Running at a speed of 3 MHz, the processing power is ample in this application.

The processor unit also includes the necessary logic, 32K of Random Access Memory (RAM) and 8K of Electrically Erasable Programmable Read Only Memory FEPROM). The former is used for variables and data logging, while the latter holds the program itself. EEPROM provides data retention while the system is off, but is electrically erasable as opposed to earlier Ultra-Violet light erasable types. This facilitates reprogramming in situ.

Interface circuit:

This section provides connection between the processor unit and the host computer that was used to develop software; downloading of programs is accomplished without interfering with normal viscometer operation.

Display:

A 6 digit 7-segment LED display and its associated decoder/driver chip provides a digital readout for the system. The display is programmable by the microprocessor and appears as six output ports. A latch has also been incorporated, such that blanking of any or all of the digits is possible: this greatly enhances the clarity of the display by allowing leaning zeros to be removed for example.

Keyboard:

A 20-key numerical membrane keypad, together with decoding logic, allows the user to control the viscometer, enter calibration viscosities, set time intervals, etc.

50Hz counter:

An 8-bit counter is clocked at the 50Hz mains frequency. By reading this input port, the microprocessor can operate a real-time clock and measure time intervals.

Timers:

Two 24-bit counters and input ports time the photo diode illumination and beam broken periods. The counters are clocked at 6 MHz; hence rotation rates down to 21 rpm may be measured, while at the motor's maximum speed of 300 rpm, the periods are accurate to about 1 part in a million (although in practice the precision of the 6 MHz crystal itself limits the accuracy to 30 parts per million).

D-A Converter:

A digital to analogue converter and latch give the microprocessor accurate control over the motor speed. A power operational amplifier buffers the output to a voltage and current sufficient to drive the DC motor. The output voltage is from 0 to $+9$ volts in 65536 steps, with a differential linearity error of only 0.001%.

Mains power supply unit:

A 12-0-12 volt toroidal transformer, rectifiers and voltage regulators form a standard power supply with $+/-$ 12 V outputs at IA for the D-A converter and buffer. A high efficiency switched mode regulator provides +5V for the digital circuits, which consume a power of approximately 5 W. Use of this unusual type of regulator results in considerably lower overall power consumption and heat dissipation.

3.3 Operating software.

A ZX Spectrum computer running an assembler application was used as a development tool, to edit and compile the operating program prior to downloading into the microprocessor control system's EEPROM. A complete listing of the viscometer control software is presented in appendix B.

A modular programming approach was adopted, and a library of subroutines for elementary functions developed (section 3.3.1). These are called from subroutines which perform statistical analysis, calculate the viscosity, control the period between measurements, and log data (section 3.3.2). These in turn are called from a main control program, under direct user control (section 3.3.3).

3.3.1 Function subroutines:

The collection of subroutines perform the basic functions listed below [ref. 6 & 7]. A 5 byte floating point format is used, consisting of a 32-hit fractional part, 8-hit exponent part, and sign bit. The numbers so represented have a range of $+/-3.4 \times 10^{0.38}$, to a precision of one part in 4.3 x 10^o9.

i) Clock/Timer: The 50Hz mains frequency counter is used to drive a real-time clock/timer, which may be displayed in either hours/minutes or hours/minutes/seconds format, according on the user's preference. The 50 Hz counter is 8-bit so in order to retain the correct time, the clock routine must be called at least every 5 seconds. In fact it is called more often, whenever the keyboard is scanned or readings taken, which in practice accounts for most of the processor's time.

ii) Input routines: These scan the keyboard, accept user input of floating point decimal numbers, and convert to the normalised binary floating point format adopted.

iii) Print routine: This allows the program to output a result to the display. The binary floating point number is converted to decimal, and leading zeros blanked.

iv) Error handling: The user is informed of any measurement or arithmetical errors that have occurred. A list of the possible error codes that may be generated is shown in table I below.

v) Arithmetic functions: These operate on numbers in normalised floating point format, and perform the following operations: addition, subtraction, multiplication, reciprocal and division.

vi) Read routines: These read the mark/space ratio and period of rotation, of the viscometer mechanism. If measurement of a viscosity outside the possible range is attempted, an appropriate error is indicated.

vii) Reset: This routine monitors the 'RST' key; if it is pressed for longer than 1/2 a second a system reset is performed. This is similar to switching the machine off and on again, except that none of the results or user defined parameters are erased, with the exception of the time and measurement interval.

viii) Regld, Regsv: These two routines load/save the Z80's registers form/to the stack (upper part of the system memory that is used as temporary storage space by the processor). They are often called at the start and finish of a subroutine, in order that the Z80's registers are preserved by the routine.

i

	Code Cause	Possible solution
E ₀	Division by zero	This could occur if a calibration viscosity of zero was entered, or if there was no calibration
E 1	PRINT overflow	The magnitude of the viscosities is too large, use a smaller unit of viscosity
E ₂	PRINT negative	\star
E_3	Viscosity too large to measure	Fit a smaller glass stirrer, or larger beaker
E ₄	Viscosity too small to measure	Fit a larger giass stirrer, or smaller beaker
E ₅	Measurement range too small	\star
E_6	FPINT conversion error	\star
E 7	FPINT negative conversion	\star
E8	Viscosity < Preset minimum	Decrease the pre-set minimum entered
E 9	Viscosity > Preset maximum	Increase the pre-set maximum entered
E A	Too many readings requested	There is only space for 6000 measurements. Enter a smaller number of measurements.

Table I: Explanation of error codes, and possible solutions. *The starred errors should not occur in normal viscometer operation

3.3.2 Viscosity measurement subroutines:

The procedure for viscosity determination is shown in the flow diagram, figure 6. First a useful measurement range is determined, by starting the motor at its maximum rate and gradually reducing the speed in steps until the displacement between the disks in the mechanism falls below 170 degrees. The lower end of the range is found by increasing the motor speed from zero until a displacement is first detected. In order that transitional oscillations in the spring or extreme damping have time to decay, five revolutions of the mechanism are allowed to pass at each speed before reading the angular displacement. Measurements near to the lower end of the range could suffer low resolution and hence inaccuracy; therefore a small amount is added here. Once these two limits have successfully been set, the processor proceeds to take ten readings of displacement angle at ten speeds equally spaced within the range. Again transitional effects are allowed to pass, by now waiting for ten revolutions before reading, at each speed. A statistical analysis [ref. 8] performs a least squares best fit on the data, to find the gradient of the graph of displacement against speed (see section 2.3). This gradient is related to that obtained from a previous calibration reading, and the viscosity calculated.

Having obtained the viscosity, it is then checked to ensure that it lies within a user specified range. If for instance if it becomes to large, no further measurements are taken. This useful function could also be used to sound an alarm if the viscosity of the test fluid deviated too greatly from a specified value. The viscosities are logged in the system memory, where there is space for up to six thousand results. After the experiment, these may be scanned by the operator.

Figure 6: Flow diagram of the subroutine for viscosity measurement.

3.3.3 Main Control Program:

The main control program is under direct control of the user, and calls the various subroutines as required. The user selects the desired operation by typing its code on the keyboard and pressing 'RUN'. A list of the available programs is shown in table 2 below. The system may be reset at any time by pressing the RST' key for longer than 1/2 a second.

The 'A' programs allow the user to enter parameters for the measurements. The time may be set (Al) and the frequency of automatic measurements specified (A2). The desired format of time display is also selectable: type 'A' for hours/minutes format, and 'B' for hours/minutes/seconds format. A calibration reading is carried out by program A3: the user must immerse the stirrer of the mechanism in a fluid of known viscosity, and type in this value (in stokes, centistokes or poise: as long as later measurements are in units consistent with this calibration). The system then performs a set of readings and calculates the gradient of the displacement/speed graph (section 3.3.2). All subsequent measurements are referenced to this value. Minimum and maximum alarm viscosities may be entered (A4), and the number of measurements required specified (A5). Note that programs A3-A5 have no default values, thus it is essential that they are run every time the system is first switched on, although not necessarily following a system reset.

The 'B' programs are for actual viscosity determination. For a oneoff measurement program B1 may be run, while for continuous viscosity monitoring B2 is used. Programs B3 and B4 are for automatic timed measurements, and both log the results in system memory. The interval between measurements, number of readings required, and range are as specified in programs A2, A5, and A4 respectively. The difference between programs B3 and B4 is that the former displays the actual time as set by A3, while the latter displays the time elapsed since the start of the experiment. This would be useful for example in lubricant oxidation experiments.

Program 'C' allows the user to scan through the recorded data, using the +/- keys. The measurement number or viscosity value may be displayed, by pressing the A or B keys respectively.

Program	Function	
A1	Set the system clock; default value 0:00	
A ₂	Specify the interval between measurements; default value 1:00	
A ₃	Perform a calibration reading using a fluid of known viscosity	
A4	Enter minimum and maximum alarm viscosities	
A ₅	Specify the number of measurements required	
B1	One-off viscosity measurement	
B ₂	Continuos viscosity measurement	
B ₃	Automatic operation, with the display showing the clock	
B4	Automatic operation, with the display showing the time elapsed	
С	Scan through the results of B3 or B4	

Table 2: Programs available to the user.

4 Experiments and results

The following experiments aimed to verify the theory (section 2) and correct operation of the viscometer, investigate the dependence of viscosity on temperature, and establish some idea of measurement accuracy.

4.1 Basic viscometer operation

4.1.1 Photo-diode Outout

The output from the photo-diode was monitored using a digital storage oscilloscope, and replayed slowly to a chart recorder, for the same fluid at three different rotation rates. The resulting graphs are shown in figure 7; note that the apparently slow rise and fall time is in fact due to the chant recorder, not the mechanism itself. The top graph shows the output while the motor is rotating at full speed, and the torque generated is sufficient to fully open the spring to an angular displacement of 180 degrees. The middle trace was taken about half way through me measurement when the rotation rate is such that the displacement is roughly 90 degrees. The lower wave form was obtained near the end of the measurement where the motor speed is low. Here there is only just enough torque to extend the spring, and the angle is very small.

From these graphs it can be seen clearly that the angular displacement of the two disks, indicated by the mark/space ratio of the wave forms, depends on the motor speed. Therefore these results provide some verification of the theory presented in section 2.3 and expectations of section 3.1.

(a): Photo-diode output at high motor speed.

(b) Photo-diode output at a medium motor speed.

(c) Photo-diode output at a low motor speed.

Figure 7: Chart recorder trace of the photodiode output at three different rotation rates. The mark/space ratio of each wave form indicates the displacement angle as a fraction of 360 degrees, while the period is that of the rotation.

4.1.2 Motor Speed during a measurement

In confirmation of the method described in section 3.3.2, figures 8-10 show the variation of motor speed with time during a measurement. The graphs were obtained with three fluids of different viscosity, and using a chart recorder to measure the voltage across the motor. Strictly speaking, due to mechanical losses in the motor, the voltage across it only approximates the speed; however this approximation is sufficient for these largely qualitative graphs. (Note that in all viscosity measurements, the microprocessor control system adjusts the motor speed using the voltage applied, but obtains the exact speed for the calculations from the optical readings.) A measurement takes around 90 seconds, depending on the test fluid's viscosity.

Figure 8: Motor speed during a calibration reading with a 1000 cst fluid

Figure 8 displays the rotation rate for the calibration reading of a 1000 cst fluid. The speed starts off at the maximum (300 rpm) and decreases slowly in steps, until the displacement angle becomes less than 170 degrees. Next the speed is increased from zero until a small angle is detected. Following this ten revolutions at maximum speed are counted, then the measurement run of ten readings equally spaced throughout the range.

Figure 9: Motor speed during measurement of a 670 cst fluid.

Figure 9 is a similar plot, obtained with a fluid whose viscosity was found to be about 670 cst. The lower viscosity results in the measurement range occurring at a generally higher speed.

Figure 10: Motor speed during measurement of a 280 cst fluid.

Figure 10 shows the same results for an even lower viscosity liquid, measuring about 280 cst. In this case even at the maximum speed the torque exerted on the glass cylinder was not enough to fully extend the spring to 180 degrees. Nevertheless as long as there is at least some displacement a measurement may still be made, as in this example. Here the fastest motor speed is used as the top end of the range, and a lower limit found in the usual way. (Such matters are transparent to the user.)

4.1.3 Angular displacement and motorspeed.

Figure 11 shows a graph of angular displacement against motor speed, for fluids of approximate viscosity 10000, 1000, and 300 cst, according to the manufacturer's specifications. The results were obtained directly from the control system, before development of the subroutines for calibration and statistical analysis. As expected the relations are linear, with a gradient which increases with viscosity.

Figure 11; Angular displacement/motor speed for 3 oils of viscosity 300, 1000, and 10000 cst

4.1.4 Conclusions

From the qualitative features of these observations, the viscometer and control system seem to function correctly and as expected. Furthermore the theoretical relations derived in section 2 also appear to be obeyed in this instrument. As expected (see section 3.1) the spiral spring appears to impose some limitations on the measurement accuracy obtainable.

4.2 Dependence of viscosity on temperature

These experiments were intended to test the approximate viscosity-temperature relation mentioned in section 2.4.2. That is,

 $v = A$ exp (Ev / k T)

where v is the kinematic viscosity, k Boltzmann's constant, T the temperature, and A and Ev constants. The measurements were obtained using both the viscometer of this project (hereafter referred to as the project viscometer), and a Ferranti-Shirley cone-on-plate viscometer. Therefore a useful comparison between the two viscometers was also obtained.

Two lubricants were tested: Dow Corning FS-1265 10000 cst lubricant, and Dow Coming DC200 1000 cst lubricant. These kinematic viscosities are stated by the manufacturer, however the temperature at which the viscosity is specified is not mentioned. However the aim of these experiments was not to determine absolute viscosities, rather to investigate the degree of temperature variation and correlation with an existing commercial viscometer. Hence both instruments were calibrated to read the stated viscosity at room temperature as a reference point.

For the project viscometer measurements, 50 cm3 of the test fluid was contained in a small beaker of diameter 4 cm. This beaker was suspended in a temperature controlled oil bath. The temperature of the test fluid itself was additionally monitored using a digital thermometer, with a thermocouple immersed in the liquid.

During the measurements ample time was allowed for the temperature to reach a stable value,

usually slightly less than that of the oil bath due to heat losses from the test fluid. Temperature control is built in to the Ferranti-Shirley viscometer, which pumps heated oil through the instrument to heat the sample under investigation.

Viscosity was measured at temperatures ranging from room temperature to about a hundred degrees centigrade. Above this temperature the oil bath becomes intolerably smelly. Numerical results are presented in Appendix 0.

Figure 12 shows in graphical form the variation with temperature of the 10000 cst fluid. Calibration was performed at 22.5C. The data from the Ferrauti-Shirley instrument approximates the exponential curve extremely well, although that from the project viscometer displays a large spread. This was probably mainly due to the inadequacies of the spiral spring. Error bars plotted on the project viscometer measurements are for a 10% random variation. Temperature is measurable to an accuracy less than half a degree, and the Ferranti-Shirley instrument specifies a precision of under 3%. Thus in the interests of clarity error bars have not been plotted on these data points.

Figure 12: Viscosity/Temperature for the FS-1265 10000 cst fluid

Figure 13 is a graph of viscosity against temperature for the 1000 cst fluid. Again the Ferranti-Shirley results appear more accurate than those of the project viscometer.

Figure 13: Viscosity / Temperature for the DC200 1000 cst fluid.

These results show that the exponential viscosity-temperature relation is well approximated within the measurement range of the experiment. This is particularly apparent for the 10000 cst FS-1265 lubricant, which displays a rapid decay of viscosity with rising temperature.

4.3 Accuracy and long term stability

In order to investigate the accuracy of the measurements end stability of the mechanism, the instrument was programmed to take 128 readings at half-hourly intervals over a continuous 64 hour period. Dow Corning DC200 1000 cst lubricant was used as the test fluid, and the calibration performed for 1000 cst at 24.1 degrees centigrade. The experiment was carried out at room temperature with no oil bath.

The instrument satisfactorily made all the measurements, a full listing of which appear in appendix D; there was no substantial drift in the instrument between start and finish. A routine statistical analysis of the data revealed a mean value of 948 cst and standard deviation of 37 cst corresponding to 4.0 % of the measured value.

The low mean value clearly demonstrates that the accuracy of all measurements cannot be better than that of the calibration: effectively the precision of the measurements is halved. In this case the calibration seems to have been high, resulting in slightly low figures for all subsequent readings.

It is thought that most of the 4 % random errors arise from the non-linearities of the spring already discussed. However viscosity is also highly affected by variations in temperature, and it could certainly be argued that blame for the observed errors could be apportioned to variations in the laboratory temperature during the day/night cycle. In order to calculate the temperature drift that would cause a +/- 4 % viscosity deviation, the coefficients obtained from the temperature experiments of section 4.2 can be used. The constants from the exponential fit of figure 13 imply that a 37 cst change on 1000 cst would require a temperature change of just 4%. Such an amount may seem excessive but certainly a substantial fraction of the deviations could be due to temperature variations of one or two degrees.

In order to determine the true effect of temperature variations on the figures. future experiments could involve accurate temperature control during the measurements, and/or logging of temperature as well as viscosity.

5 Discussion

Several modifications and enhancements have been foreseen, some of which are discussed here. These further developments would be possible in the mechanism, microprocessor control system, and operating software.

Mechanism:

The mechanism performed well with the exception of the spiral hair spring. Improving this component would undoubtedly result in considerably greater measurement accuracy. A properly machined spring would need to be custom manufactured for this purpose, as none are currently commercially available.

Another problem that was experienced was that the chuck wobbled due to imperfections in the pinjoint between parts (F)and (G) in figure 3; this joint is necessary to enable the mechanism to be assembled. It is thought that a tapped hole in (F) and screw-like end to (G) would result in a screw joint that would substantially reduce this problem.

Mounting the entire mechanism in a rigid frame, and making provision for the test fluid beaker to be held securely beneath it, would eliminate the need for a clumsy retort stand. The experimental conditions would be easier to set up and reproduce accurately.

Microprocessor control system:

As mentioned temperature variations have a large effect on viscosity; therefore some means of temperature control would be advantageous. This function could be incorporated into the existing circuit, by using the digital to analogue converter and an additional comparator to perform analogue to digital conversion of the output voltage from a thermocouple. The processor would extract the temperature from this and compare it with an existing user-specified value. A heater immersed in the fluid and under control of the processor would maintain the liquid at a steady temperature. This modification would greatly enhance the viscometer's usefulness by making the measurements more precise; in addition, temperature-viscosity curves could be obtained automatically by the processor.

Another worthwhile addition would be some form of analogue output, suitable for driving a chart recorder for example. Again the digital to analogue converter could be utilised, followed by a sample-and-hold amplifier so that ordinary motor speed control is not prevented.

A computer interface for PCs and Macintoshes would allow data logging and manipulation if desired. The tedium of copying by hand the 128 results of section 4.3, then typing them all into a calculator, illustrates the obvious advantages of using a computer to handle such mundane tasks. Such an interface could easily be added to the existing circuit, and need not prevent the viscometer's operation as a stand alone unit when desired.

Operating software:

Functional subroutines were developed in an extremely logical manner, which facilitates easy alterations to the operating software. In addition to the modifications required to allow the improvements discussed above, further programs could be incorporated to perform more functions, such as error analysis for example. Compensations for non-linearity or losses in the mechanism

can be applied using a polynomial fit to the data, as opposed to the least squares straight line best fit that was used here. This could also be arranged to permit the testing of non-Newtonian fluids (see section 2.2).

Microprocessor control is extremely versatile and many program improvements or application specific requirements may be implemented with ease.

6: Conclusion

The theories of viscosity measurement and temperature dependence considered in section 2 of this report have been verified, and the results additionally used to compare the viscometer's performance against that of a commercially available type, the Ferranti-Shirley cone-on-plac viscometer.

The viscometer developed exceeded expectations in some respects. In particular the versatility of microprocessor control in scientific instruments has become more apparent. The precision of the device was not as high as at fust hoped, although considerably better than that of the original viscometer briefly described in the introduction. It is strongly expected that the blame for this shortcoming lies solely with the inadequate spiral spring, and replacement of this item with a more accurate component should result in immediate and substantial improvements in the precision of the instrument.

Some improvements have been envisaged and the potential of the device demonstrated; it is hoped that these justify further development The instrument should satisfy the requirement for monitoring bulk viscosity in oxidation tests, and with the enhancements suggested, perhaps also be of use in many other applications.

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Pinouts for the integrated circuits and allocation of the interface and mechanism connector sockets.

Microprocessor, memory, keyboard and display.

D/A converter, power supply, power amp, photo-diode.

Timers.

APPENDIX B: ASSEMBLY PROGRAM LISTING:

Contents:

E2PROM Program Order of Subroutines Constants Definition Variables Definition Keycodes

Program Listing:

The E2PROM is programmed by reversing the positions of IC2 and IC3, and switching both S1 and S2 to 'ON'. The following program is run from RAM, with the subroutines immediately following. To check correct writing, it may be run again with S2 switched to 'OFF'. The location where any error occured will be displayed.

Variables Definition:

Keycodes:

 LDIR ; Transfer first number into Mltbuf for addition. LD A,(HL) ADD A,128 LD (MULTE),A ; Multe holds the exponent part. POP DE LD L,E LD H,D LD BC, 4
LD DE.M DE, MLTBUF+12 LDIR ; Transfer second number into Mltbuf for addition. LD IX,MLTBUF JR Z, ADD2 SET 0, (IX+16) ADD2 BIT 7,(IX+15) JR Z, ADD3 SET 1, (IX+16) ; Test the sign bits and use the last byte of Mltbuf to store thme in. Now these sign bits are set to 1 as assumed by the floating point format. ADD3 SET 7,(IX+7) SET 7, (IX+15) LD A,(HL) ADD A,128 LD B,A LD A,(MULTE) SUB B JR Z,ADD7 ; Compare the two exponents to see which is least; if they are equal then the shifting stage can be skipped. JR NC,ADD4 LD IX,MLTBUF NEG LD HL,MULTE LD (HL), B JR ADD5 ADD4 LD IX,MLTBUF+8 ADD5 LD B,A ; After selecting the appropraite number for exponent equalistaion, shift in zeros until the exponents become equal. Now the fractional parts may be added. ADD6 SRL (IX+7) RR $(IX+6)$ RR (IX+5) RR $(IX+4)$ RR (IX+3) RR $(IX+2)$ RR $(IX+1)$ RR (IX) DJNZ ADD6 ADD7 LD IX,MLTBUF LD $A, (IX+16)$ OR A ; If both sign bits are positive call Add12 to add the fractional parts. CALL Z,ADD12 CP 1 ; If one or other sign bits was negative then the sign flag holds 1 or 2 and a subtraction must be performed not an addition. Add16 does this, IX and IY hold the two numbers in the correct order depending on which sign was negative. JR NZ,ADD8 LD IX,MLTBUF LD IY,MLTBUF+8 CALL ADD16 ADD8 CP 2

 JR NZ,ADD9 LD IX,MLTBUF+8 LD IY,MLTBUF CALL ADD16 ADD9 CP 3 JR NZ,ADD10 ; If both sign bits were negative then an addition is needed. CALL Z, ADD12 SET $7, (IX+7)$ ADD10 LD IX,MLTBUF+4 POP HL LD B, 4 ADD11 LD A,(IX) LD (HL),A INC IX INC HL DJNZ ADD11 ; Transfer the result to the correct location. LD A,(MULTE) SUB 128 LD (HL),A ; Store the exponent part at the result location, thus completing the addition operation. CALL REGLD RET ; This subroutine adds the fractional parts and normalises the result. Note that following addition, the normalisation process is simply a possible 1-bit shift. ADD12 LD IX,MLTBUF+3 LD IY,MLTBUF+11 LD B, 5 ADD13 LD A,(IX) ADC (IY) LD (IX), A
TNC IX INC INC IY DJNZ ADD13 JR NC,ADD15 LD IX,MLTBUF+7 LD $B, 5$; Normalise if necessary by shifting the result and incrementing the exponent. ADD14 RR (IX)
DEC IX DEC DJNZ ADD14 LD HL,MULTE INC (HL) ADD15 LD IX,MLTBUF RES $7, (IX+7)$ LD $A, 9$ RET ; This subroutine subtracts the fractional parts, pointed to by IX and IY. ADD16 LD B,8 ADD17 LD A,(IY) SBC (IY) LD (IX), A
LD (IY). A (IY) , λ INC IX
INC TY T_{NC} DJNZ ADD17 JR NC,ADD19 LD IX,MLTBUF LD B,8 ; In the case of a negative result, complement the fraction to make it positive and adjust the sign bit accordingly. ADD18 LD A,(IX)
CPL LD (IX),A INC IX DJNZ ADD18 LD IX,MLTBUF-8 ; Call subroutine Norm to normalise the result. CALL NORM SET 7, (IX+15) ; Set the sign bit indicating a negative result. $LD \tA, 9$ RET ADD19 LD IX,MLTBUF-8 CALL NORM ; Reset the sign bit indicating a positive result.; then call subroutine Norm to normalise the result. RES 7,(IX+15) $LD \tA, 9$ RET Routine: Alarm Function: Check to see if next measurement is due yet Called by: pb3 Calls: None Entry: None Exit: Nxtsec adjusted if necessary; Z flag set if due Preserved: None ALARM LD IX,NXTSEC LD IY,CLKSEC LD B, 6 ALM1 LD A,(IX) CP (IY) RET NZ ; Compare the alarm time with the current time and return with NZ flag set if they are not yet equal. INC IX INC IY DJNZ ALM1 ; If a measurement is due then compute the next alarm time. ALM2 LD IX,NXTSEC LD IY,CLKSEC LD HL,LMMIN LD $A, (IY)$ LD (IX),A INC IX INC IY LD A,(IY) LD (IX),A ; The next alarm time has the same seconds value as the current time. Now the alarm period minutes and hours (held in Lmmin and Lmhrs respectively) are added to the current time. Checks are made to ensure that the if the number of minutes overflows then ten is subtracted and the 10s of minutes variable adjusted accordingly, and so on for the other numbers. TNC TX INC IY LD $A, (IY)$ ADD A,(HL)

 JR C,ALM3 SUB A,10

CP 10

ALM3 CCF

Routine: Almset Function: Get measurement period from the user. Called by: Main Calls: Keyb Entry: None Exit: Period is stored in lmmin, lmhrs

Preserved: None

ALMSET XOR A LD IX,PRIBUF ; Space at Pribuf is used for temporary storage space. The old measurement period is displayed so that the user can modify it or continue, as required. LD $A, (LMHRS+1)$ OUT (12),A LD A,(LMHRS) OUT (11),A LD $A, (LMMIN+1)$ OUT (9),A LD A,(LMMIN) OUT (8),A ALMST1 LD A,(CLKDOT) ; The use of the Clkdot variable permits the current digit to be flashed at 1 Hz, similar to a cursor, using the display blanking register, Out 144. OR A LD A,54 JR NZ,ALMST2 DEC A DEC A ALMST2 OUT (144), A CALL KEYB CP 21 RET Z ; Return from the subroutine if the Enter key is pressed. LD E,10 CP 2 JR NZ,ALMST3 LD E, 4 ; The E register is used to check the hours digit, which must be less than 4 if the 10s of hours is 2, less than 10 otherwise. ALMST3 CP 3 JR NC, ALMST1 OUT (12),A LD (LMHRS+1),A ; The 10s of hours are stored at Lmhrs+1; subsequent digits are store at Lmhrs, Lmmin+1 and Lmmin respectively. The following sections use the same general format for measurement period entry and checking. OR A LD A,54 JR NZ,ALMST4 DEC A DEC A ALMST4 LD (IX),A ALMST5 LD A,(CLKDOT) OR A $LD \tA, (IX)$ JR NZ,ALMST6 SUB A, 4 ALMST6 OUT (144), A CALL KEYB CP 19 ; If the Clr key is pressed the subroutine is started again.
JR z, ALMSET Z, ALMSET CP 21 RET Z CP E JR NC,ALMST5 OUT (11),A LD (LMHRS),A ALMST7 LD A,(CLKDOT)

 LD HL,CALVIS CALL INPUT ; Get the calibration viscosity value from the user. CALL PRINT LD HL,VISCTY CALL VISC ; Call subroutine Visc to measure the raw uncalibrated viscosity. RET C LD BC,CALVIS LD DE,VISCTY LD HL,CALVIS CALL DIVIDE ; Calculate the viscosity calibration multiplier. CALL REGLD RET Routine: Chk1 Function: Finds the maximum motor speed, where angle > 170. Called by: Range Calls: Error, Read, Sub Entry: None Exit: Mtrmax is set; C flag set on error Preserved: None CHK1 XOR A LD (MTRMAX),A OUT (142),A OUT (143),A ; Start at the maximum motor speed, ie output zero to the DAC. LD DE,NUM4 LD HL,NUM5 LD B,10 CALL READ Do ten revolutions initially to get the motor up to speed. JR NC, CHK1C CHK1A LD A, (MTRMAX)
OUT (143), A (143) , A LD DE,NUM4 LD HL,NUM5 LD $B, 3$; 3 revolutions per subsequent reading. CALL READ JR NC,CHK1C ; On error jump. LD BC, NUM4 LD DE,ONE70 LD HL,NUM1 CALL SUB ; Subtract 170 degrees to see if the measured angle is < 170. LD IX,NUM1 BIT 7, (IX+3) JR NZ,CHK1B ; If angle > 170 then decrease the motor speed and try again. LD A, (MTRMAX)
ADD A.8 A, 8 LD (MTRMAX),A JR CHK1A CHK1B LD A,255 OUT (143), A ; Stop the motor and return. OR A

 RET CHK1C LD A,255 OUT (143),A ; Decide the cause of the error: viscosity too small or too large. Call subroutine Error to display the error code. LD A, (MTRMAX) OR A LD $A, 4$ JR Z, CHK1D LD $A, 3$ CHK1D CALL ERROR SCF RET Routine: Chk2 Function: Finds the minimum motor speed, where angle > 0. Called by: Range Calls: Read6 Entry: None Exit: Mtrmin is set Preserved: None CHK2 LD A,(MTRSPD) LD (MTRMIN),A ; Start at the minimum motor speed specified by the constant, Mtrspd. Below this speed the motor will not turn at all. XOR A OUT (142), A CHK2A LD A,(MTRMIN) OUT (143),A LD B, 5 ; 5 revolutions per reading. $CHK2B$ IN A , (6) LD (TIMERB),A ; Initialise timer; Read6 is used to check that 2 seconds have not passed. If no angle is seen in this time, it is assumed that the current speed is too slow, and a jump is made. CHK2C CALL READ6 JR NC,CHK2F IN A,(14) RL A JR C,CHK2C IN A, (6) LD (TIMERB),A CHK2D CALL READ6 JR NC, CHK2F
IN A. (14) $A, (14)$ RL A JR NC,CHK2D DJNZ CHK2B CHK2E LD A,255 OUT (143),A ; Stop motor and return when a non-zero angle has been measured. RET CHK2F LD A, (MTRMIN) SUB A, 8 LD (MTRMIN),A ; Increase motor speed and try again. JR Z, CHK2E JR CHK2A

Routine: Chk3 Function: Checks that minimum motor speed < maximum motor speed Called by: Range Calls: Error Entry: Mtrmin, Mtrmax have been set by Chk1 and Chk2 Exit: C flag is set on error Preserved: None CHK3 LD A,(MTRMAX) LD B,A LD A,(MTRMIN) SUB A, 8 ; Make sure that the difference between the maximum and minimum motor speeds is positive and greater than 8. CP B JR Z, CHK3A JR C,CHK3A RET CHK3A LD A,5 ; Signal an error if the range is too small or the minimum speed greater than the maximum speed. CALL ERROR SCF RET Routine: Clkset Function: User sets clock
Called by: Main Called by: Main
Calls: Kevb Calls: Keyb
Entry: None Entry: Exit: New time is in clksec, clkmin, clkhrs, and 50Hz counter is reset Preserved: None CLKSET LD IX,PRIBUF LD IY,CLKSEC LD B, 6 LD C, 8 XOR A CLKSTO OUT (C), A INC C LD (IX),A LD (IY),A INC IX INC IY DJNZ CLKST0 ; Use Pribuf as temporary storage space and initialise all the time digits to zero, i.e midnight. LD IY, CLKFLG
LD (IY).2 (TY) , 2 CLKST1 LD A,(CLKDOT) ; Use of the Clkdot variable allows the current digit to be flashed at 1 Hz, similar to a cursor, using the digit blanking register, out 144. OR A LD A,54 JR NZ,CLKST2 DEC A DEC A

CLKST2 OUT (144), A CALL KEYB CP 21 JP Z,CLKSTF ; If the Enter key is pressed, jump to the end. LD E,10 CP 2 JR NZ,CLKST3 LD $E, 4$; Use of the E register here allows the Hours to be checked according to the 10s of hours entered: if 2 is entered then the Hours must be less than 4, otherwise less than ten. The other digits are entered and checked in a similar way. CLKST3 CP 3 JR NC, CLKST1 OUT (12),A LD (CLKHRS+1),A OR A LD A,54 JR NZ, CLKST4 DEC A DEC A CLKST4 LD (IX),A CLKST5 LD A,(CLKDOT) OR A $LD \qquad A, (IX)$ JR NZ, CLKST6 SUB $A, 4$
OUT $(144), A$ CLKST6 OUT CALL KEYB CP 19 JR Z, CLKST1 ; If the Clr key is pressed, move to the 10s of hours digit again. CP 21 JP Z,CLKSTF CP E JR NC, CLKST5 OUT (11),A LD (CLKHRS),A CLKST7 LD A,(CLKDOT) OR A $LD \qquad A, (IX)$ JR NZ, CLKST8 SUB A,16 CLKST8 OUT (144), A CALL KEYB CP 19 JR Z, CLKST1 CP 21
JR $2, 0$ Z, CLKSTF CP 6 JR NC, CLKST7 OUT (9),A LD $(CLKMIN+1)$, A CLKST9 LD A,(CLKDOT) OR A LD $A, (IX)$ JR NZ,CLKSTA SUB A,32 CLKSTA OUT (144), A CALL KEYB CP 19 JP Z, CLKST1 CP 21 JP Z,CLKSTF

 CP 10 JR NC, CLKST9 OUT (8), A LD (CLKMIN),A LD A,10 OUT (13),A INC (IX)
CLKSTB LD A, (C) A, (CLKDOT) OR A $LD \tA, (IX)$ JR NZ,CLKSTC DEC A CLKSTC OUT (144), A ; Get the time display format: an A entered here (default) will put the clock in Hours . Minutes mode, while B puts it in Hours.Minutes.Seconds mode. CALL KEYB CP 19 JP Z, CLKST1 CP 21 JP Z, CLKSTF CP 10 JR NZ,CLKSTD OUT (13),A LD (IY), 2 JR CLKSTE CLKSTD CP 11 JR NZ,CLKSTB OUT (13),A LD (IY),1 JR CLKSTE CLKSTE JP CLKST1 ; Go back to the 10s of hours digit in case any digit needs to be changed by the user. $CLKSTF IN A, (6)$ LD (CLK50), A XOR A LD (CLKSEC),A LD (CLKSEC+1),A ; Reset the 50 Hz counter and initialise the seconds and tens of seconds to zero, then return. RET Routine: Clock Function: Updates clock and displays it if the appropriate flag is selected Called by: Keyb, Read Calls: Reset Entry: Clkflg=0 for no display, 129 for Hrs.Mins.Secs format, 130 for hrs mins format. Exit: None Preserved: E, IX, IY CLOCK CALL RESET ; Call the Reset subroutine to execute a system reset if the Reset key is being pressed. CALL CLK5 ; Check the 50 Hz counter, and update the clock if necessary. CP 25 JR C,CLK ; If 0.5 seconds have passed since the beginning of the second, clear Clkdot: this is used later to flash the decimal point between the Hours and Minutes in

format A. XOR A LD (CLKDOT), A
CLK LD A, (CLKFLG) LD A, (CLKFLG) BIT 7,A RET Z ; Return if clock display is not required. AND 3 CP 2 JR Z, CLK1 ; Display in format B, if Clkflg is 130, otherwise branch to Clk1 and display in format B. LD A,(CLKSEC) OUT (8), A LD A,(CLKSEC) OUT (9),A LD A,(CLKMIN) OR 16 ; Or 16 illuminates the decimal point of the digit. OUT (10),A LD A,(CLKMIN+1) OUT (11),A LD A,(CLKHRS) OR 16 OUT (12),A LD A , (CLKHRS+1)
OUT (13) , A (13) , A OR A LD A,254 JR Z, CLKO INC A CLK0 OUT (144),A RET CLK1 LD A,(CLKMIN) OUT (8),A LD A,(CLKMIN+1) OUT (9),A LD A,(CLKHRS) LD B,A LD A,(CLKDOT) OR B ; Include a decimal point here only in the first half of each second. OUT (11),A LD A,(CLKHRS+1),A OUT (12),A OR A LD A,52 JR Z, CLK2 INC A
INC A INC CLK2 OUT (144),A RET CLK3 LD HL,CLKSEC ; This part of the subroutine increments the time by one second. Minutes and hours are also updates if the seconds overflow. LD $C, 10$
LD $D, 6$ $D,6$ LD B, 0 LD A,C INC (HL) CP (HL) RET NZ LD (HL),B INC HL

Preserved: All DIVIDE CALL REGSV PUSH HL LD HL,PRIBUF ; Use Pribuf as temporary storage space; calculate the division by first calculating the reciprocal of the quotient then multiplying by the divisor. CALL RECIP POP HL
LD DE DE, PRIBUF CALL MULT RET Routine: Equals Function: Set a floating point number equal to another Called by: Pb3, Visc Calls: Regld, Regsv

Entry: DE points to DE points to $#1$, HL to $#2$. $Exit:$ $#1=#2$ Preserved: All EQUALS CALL REGSV LD BC,5 LDIR CALL REGLD RET Routine: Err Function: Display error message Called by: Error, Print Calls: None Entry: A holds error code Exit: None Preserved: B, C, D, E, H, L, IX, IY ERR PUSH AF AND 15 OUT (8), A LD A,14 OUT (13),A LD A,33 OUT (144),A POP AF SRL A SRL A SRL A SRL A OR A RET Z ; The error code is a single byte. The lower 4 bits are displayed at the right of the display; if the higher 4 bits are zero the digit is not displayed. OUT (9) , A

I.D $A.49$ A, 49 OUT (144),A RET

Routine: Error Function: Displays error message and waits for a key to be pressed
Called bv: Chkl, Chk3, Fpint, Measno, Recip, , Vischk Called by: Chk1, Chk3, Fpint, Measno, Recip, , Vischk
Calls: Err, Wait Calls: Err, Wait
Entry: A holds e A holds error code Exit: A holds key code Preserved: IX, IY, E ERROR CALL ERR ; Call subroutine Err to display the error, then Wait to pause until a key is pressed. CALL WAIT RET Routine: Fpint Function: Converts a floating point number to a two byte integer. The FP number must be positive and <65536. Called by: Measno, Visc Calls: Error Entry: IX points to FP number Exit: HL holds the integer part Preserved: None FPINT LD B , (IX+4) LD , $(X+3)$ LD $E, (IX+2)$ LD $H, (IX+1)$ LD L , (IX) LD A,B ; Read the floating point number into the Z80 registers. CP 17 JR C,FPINT1 CP 128 JR C, FPINT4 ; If the floating point number is too big then jump to fpint4 and signal error code 6; otherwise if it is zero, set HL to zero and return. LD L,0 LD H,L RET FPINT1 BIT 7, D JR NZ, FPINT5 ; If negative, signal error 7. The rest of the routine is just shifting until the exponent becomes zero. INC B XOR A LD C,A SET 7, D JR FPINT3 FPINT2 RL L RL H RL E EL D RL C RL A FPINT3 DJNZ FPINT2 ; Load the integer part of the floating point number into HL, and return. LD L,C LD H,A RET FPINT4 LD A, 6

 CALL ERROR RET FPINT5 LD A, 7 CALL ERROR RET Routine: Init Function: Initialises certain variables
Called by: Called automatically straight Called by: Called automatically straight after a System Reset.
Calls: Follows into Main Follows into Main
None Entry: Exit: None Preserved: None ; The alarm period is set to its default value of 1 hour, and the time is set to midnight.
INIT L LD A, 255 OUT (142),A OUT (143), A ; Stop the motor. IN $A_{\ell}(6)$ OUT (CLK50), A LD A,16 LD (CLKDOT),A ; Set Clkdot for the start of a second. XOR A LD (CLKFLG),A LD (LMMIN),A LD (LMMIN+1),A ÖD (LMHRS+1),A LD (CLKSEC),A LD (CLKSEC+1), A LD (CLKMIN),A LD (CLKMIN+1), A LD (CLKHRS),A LD (CLKHRS+1), A

INC A INC LNC ...
LD (CLKFLG), A ; The clock is started in format B. IN A_{1} (6) LD (CLK50),A ; Reset the 50 Hz counter. MAIN Routine: Input Function: Get a number from the user and convert it into Floating point format Called by: Almvis, Calib, Measno Calls: Keyb, Mult, Regld, Regsv Entry: HL points to variable's location Exit: Input variable stored at HL
Preserved: All Preserved: All INPUT CALL REGSV PUSH HL INP0 LD B,5 LD A,255 LD HL,INPBUF

; Use storage space at Inpbuf as temporary space. INP1 LD (HL),A INC HL
DJNZ INP1 $DJNZ$; Clear the storage space. LD (HL),0 $LD \tA, 2$ LD (INPDGT),A ; Inpdgt holds the number of digits entered +2. LD IX,INPBUF LD $A, (IX+5)$ JR INP7 INP2 CALL KEYB CP 255 JR Z, INP2 ; Detect a keypress and see if it is a decimal point: if not then jump to Inp4. CP 17 JR NZ, INP4 LD HL,INPDGT BIT 7, (HL) JR NZ, INP2 ; If 6 digits have already been entered then allow no more! SET $7, (HL)$ LD A,(HL) CP 130 JR NZ, INP3 INC (HL) INP3 SET $4, (IX+5)$; Enter a decimal point. JR INP2 INP4 CP 21 JR Z, INPENT ; 'Enter' causes a jump to the conversion part of the subroutine, 'Clr' causes the input buffer to be cleared. CP 19 JR Z, INPO CP 10 JR P, INP2 ; Do not allow a non-numeric keypress. OR A JR NZ, INP5 ; A zero entered requires special treatment depending on whether or not it is the first digit to be entered, in which case it is ignored. LD D,A LD A,(INPDGT) CP 2 JR Z, INP2 LD A, D
INP5 LD HL, LD HL, INPDGT BIT $3,(HL)$; If 6 digits have already been entered then allow no more! Otherwise increment the number of digits flag. JR NZ, INP2 INC (HL)
I.D HI.T HL, INPBUF+5 LD D,A LD A,(INPDGT) CP 3 JR NZ, INP6 LD (HL),255 INP6 LD A,D LD HL,INPBUF LD DE,INPBUF LD BC, 5

 INC HL LDIR ; Shift the digits in the display buffer left to make room for the typed digit. LD $(IX+5)$, A LD HL,INPDGT BIT $7, (HL)$ JR NZ, INP8 INP7 OR 16 INP8 LD C,8 LD B, 6 LD HL,INPBUF+5 INP9 OUT (C),A RL A RL D INC C DEC HL LD A,(HL) DJNZ INP9 ; Display all the digits in the display buffer. LD A,D CPL OUT (144),A ; Set the digit blanking register according to digits entered. Note that initially the input buffer contains 255s; these are rotated into the D register in the above loop, which after inversion gives the correct value to be sent to the digit blanking register. JP INP2 INPENT LD HL,0 ; Conversion of data in the input buffer to floating point format. LD D,H LD E,H LD IX,INPBUF LD B, 6 LD C, 0
INP10 PUSH BC PUSH BC LD A,(IX) INC IX CP 255 JR NZ, INP11 XOR A ; Enter zeros for 255s in the input buffer. INP11 BIT $4, A$ JR Z, INP12 ; Detect the decimal point when it occurs and save its location in the C register for later use. POP BC LD C,B DEC C
PUSH BC PUSH BC
AND 15 AND ; The following is the actual decimal to binary conversion for 1 digit; it is repeated 6 times for the entire input buffer. INP12 CALL INPSHF LD (INPHI), DE
LD (INPLO).HL LD (INPLO), HL
CALL INPSHE INPSHF
TNPSHF CALL₁ LD BC,(INPLO) ADD HL,BC EX DE,HL LD BC,(INPHI) ADC HL,BC EX DE,HL LD C,A

 LD B,0 ADD HL,BC JR NC, INP13 INC E
POP BC $INP13$ DJNZ INP10 ; Repeat the conversion 6 times: the counter is held in the B register. LD B,32 XOR A OR L
OR H OR H
OR E OR JR NZ, INP15 ; If zero was entered, the following section inserts a floating point zero at the desired input variable location, then returns. Floating point zero is defined as 0,0,0,0,128. For non-zero numbers jump to Inp15. POP HL LD B, 4 INP14 LD (HL),0 INC HL DJNZ INP14 LD (HL),128 CALL REGLD RET ; Normalise the number. INP15 SLA A RL RL E RL D DEC B BIT 7,D LD (INPBUF),HL LD (INPBUF+2), DE LD A,B LD (INPBUF+4),A LD B,C LD A,B OR A JR Z, INP17 ; If an integer was entered then no multiplications are necessary (jump to Inp17); otherwise multiply by a tenth, C number of times, to take account of the position of the decimal point in the input buffer. INP16 PUSH BC LD BC,INPBUF LD DE,TENTH LD HL,INPBUF CALL MULT POP BC
DJNZ INP16 DJNZ
POP INP17 POP HL LD IX,INPBUF LD B, 5 $INP18$ LD $A, (IX)$ LD (HL), A
TNC HL HL
IX TNC DJNZ INP18 ; Transfer the result to the desired variable location specified by HL and return. CALL REGLD RET INPSHF ADD HL,HL EX DE,HL ADC HL,HL

EX DE,HL

; This subroutine shifts the DE and HL register pairs by 1 bit left. RET

Routine: Intfp Function: Converts a two byte positive integer to floating point format. Called by: Pc, Range. Calls: None Entry: HL holds the integer, IX points to the Floating point variable.
Exit: FP stored at IX FP stored at IX
None Preserved: INTFP XOR A OR H OR_L JR NZ, INTFP1 ; If the number to be converted is zero, enter the floating point zero, defined as 0,0,0,0,128, and return. LD B,128 JR INTFP3 INTFP1 LD B,16 ; Rotate the integer, decreasing the exponent, until the leftmost bit is a 1. INTFP2 BIT 7,H JR NZ, INTFP3 ADD HL,HL DEC B JR INTFP2 INTFP3 RES 7,H LD $(IX+4)$, B LD $(IX+3)$, H LD $(IX+2)$, L XOR A LD $(IX+1)$, A LD $(IX+0)$, A ; Store the floating point number at the specified location. RET Routine: Keyb Function: Detect a keypress and update the clock Called by: Almset, Clkset, Input, Main, Pb3, Pc, Wait Calls: Clock Entry: None Exit: A holds keycode Preserved: IX, IY, E KEYB CALL CLOCK ; Update the clock each time Keyb is called. LD C,8 LD D,0 LD L,255 ; Scan the keyboard matrix.
KEYBO TN A. (C) IN $A, (C)$ OR 224 255 JR Z, KEYB3 ; If no key in row C is pressed, then go to the next row, otherwise find out which key was pressed, by rotating until a '0' is found. LD B, 5 KEYB1 RR A

 JR C,KEYB2 LD H,A LD A,255 CP L ; Check that this is the first key detected. If more than one key is pressed then jump to Keyb7, i.e disregard them all. JR NZ, KEYB7 LD L,D LD A,H KEYB2 INC D DJNZ KEYB1 KEYB3 LD A,5 ADD D LD D,A LD A,12 INC C CP C JR NZ, KEYBO ; Return to Keyb0 to scan a new row if they have not all been scanned already. LD A,(KEYLST) CP L JR NZ, KEYB4 ; Check that the currently pressed key is not the same as the previous key. If it is then return 255, i.e no key pressed. This prevents auto-repeating. LD A,255 RET KEYB4 LD A,L LD (KEYLST),A ; Store the new keynumber and wait for 3/50 of a second. This effectively debounces the key. IN A , (6) LD D,A KEYB5 IN A , (6) SUB D JP P,KEYB6 NEG KEYB6 CP 3 JR C,KEYB5 LD A,255 CP L RET Z ; Return if no keys were pressed, otherwise add the keynumber to the start address of the list of keycodes and fetch the keycode. LD BC,KEYS LD H,0 ADD HL,BC LD A,(HL) CP 16 ; Check that the pressed key was not Rst, if it was then jump to Keyb7 and return 255, i.e no key pressed. A Rst keypress requires special treatment and is detected by the subroutine Reset. JR Z, KEYB7 RET KEYB7 LD A,255 RET Routine: Main Function: Main driver routine Called by: Preceded directly by Init Calls: Almset, Almvis, Calib, Clkset, Keyb, Meas, Measno, Pb2, Pb3, Pb4, Pc, Print, Wait Entry: None

Exit: None Preserved: None MAIN LD IX,CLKFLG SET $7, (IX)$; Enable the clock display. CALL WAIT ; Wait for a keypress, disable clock display, and see if the key was 'A'. If not jump to Main6. RES 7,(IX) CP 10 JR NZ, MAIN6 OUT (13),A LD $A, 1$ OUT (144),A MAIN1 CALL KEYB CP 19 ; If the Clr key is pressed then restart. JR Z, MAIN LD B, 1 CALL MAIN13 ; Calling the Main13 subroutine checks the next character entered to see if its a 1, if so then subroutine Clkset is called. JR NZ, MAIN2 CALL CLKSET JR MAIN MAIN2 LD B,2 CALL MAIN13 JR NZ, MAIN3 ; Program A2, set measurement period. CALL ALMSET JR MAIN MAIN3 LD B,3 CALL MAIN13 JR NZ, MAIN4 ; Program A3, Calibrate. CALL CALIB JR MAIN MAIN4 LD B,4 CALL MAIN13 JR NZ, MAIN5 ; Program A4, Set measurement range. CALL ALMVIS JR MAIN MAIN5 LD B,5 CALL MAIN13 JR NZ,MAIN1 ; Program A5, Get number of measurements. CALL MEASNO JR MAIN
CP 11 MAIN6 CP ; Check if key was 'B', if not, jump. JR NZ, MAIN11
OUT (13). A (13) , A LD $A, 1$
OUT (14) (144) , A MAIN7 CALL KEYB CP 19 JR Z, MAIN LD B,1 CALL MAIN13 JR NZ,MAIN8 ; Program B1, one-off viscosity measurement.

LD HL, VISCTY
CALL MEAS MEAS CALL PRINT
CALL WAIT CALL JP MAIN MAIN8 LD B,2 CALL MAIN13 JR NZ, MAIN9 ; Program B2, continuous viscosity measurement. CALL PB2 JP MAIN MAIN9 LD B,3 CALL MAIN13 JR NZ, MAIN10 ; Program B3, timed viscosity measurements, clock shows real time. CALL PB3 JP MAIN MAIN10 LD B,4 CALL MAIN13 JR NZ, MAIN7 ; Program B4, timed viscosity measurements, clock shows time elapsed since start of experiment. CALL PB4 JP MAIN MAIN11 CP 12 ; Check if the key pressed was 'C', if not, start Main again. JP NZ,MAIN OUT (13),A LD $A, 1$ OUT (144), A MAIN12 CALL KEYB CP 19 JP Z,MAIN C 22 JR NZ, MAIN12 ; Program C, scan through results. CALL PC JP MAIN MAIN13 CP B ; Subroutine Main13 checks the entered key against the code held in the B register and returns if not equal. If equal it waits until the Run key is pressed. RET NZ OUT (12),A LD $A, 3$ OUT (144),A MAIN14 CALL KEYB CP 19 JR NZ,MAIN15 ; If Clr key pressed, Pop AF to restore the stack, and jump to the start of Main. POP AF
JP MA MAIN MAIN15 CP 22 RET Z JR MAIN14 Routine: Mark Function: Counts "Mark" of the Mark/Space ratio Called by: Read Calls: None Entry: HL points to the location mark will be stored at

Exit: Mark stored at HL Preserved: None MARK IN A , (3) LD E,A IN $A, (4)$ LD D,A IN A , (5) LD C,A ; Input the counter values through ports 3, 4 and 5. LD B,24 XOR A MARK1 BIT 7, C JR NZ,MARK2 ; Normalise by shifting left until the leftermost bit is a 1. SLA E RL D RL C DEC A DJNZ MARK1 MARK2 RES 7, C ; Store the result at HL. LD (HL),0 INC HL LD (HL),E INC HL LD (HL),D INC HL LD (HL), C INC HL LD (HL),A RET Routine: Meas Function: Actual viscosity measurement Called by: Main, Pb2, Pb3 Calls: Mult, Regld, Regsv, Visc Entry: HL holds address viscosity is to be stored at Exit: Viscosity stored at HL; C flag is set on error
Preserved: All Preserved: MEAS CALL REGSV CALL VISC ; Raw viscosity measurement. RET C LD B,H LD C,L LD DE,CALVIS ; Multiply by the calibration coefficient. CALL MULT CALL REGLD RET Routine: Measno Function: Get from the user the number of readings required and check that its not too many Called by: Main Calls: Error, Fpint, Input Entry: None

Exit: lognmx holds number of measurements required Preserved: None MEASNO LD HL, NUM1 CALL INPUT ; Get the number from the user. PUSH HL
POP IX POP CALL FPINT ; Convert from floating point to two byte integer. LD (LOGNMX),HL LD DE,LOGMAX OR A SBC HL,DE ; Subtract maximum number of measurements allowed and return if less, otherwise indicate error A, and get another value. RET C LD A,10 CALL ERROR JR MEASNO Routine: Mlt Function: Multiplies two 32-bit positive integers Called by: Mult, Print Calls: None Entry: $#1$ in Mltbuf $0-3$, $#2$ in Mltbuf $4-7$ Exit: Result in M1tbuf 8-15 Preserved: C, D, E, H, L, IY MLT LD IX, MLTBUF XOR A LD $(IX+8)$, A ÖD (IX+9),A ÖD (IX+10),A LD $(IX+11)$, A ; Clear space for result bytes 0-3. LD B,32 ; In the following loop, 32 bit multiplication is acheived by repeatedly shifting the result/multiplier and adding the multiplicand if a 1 is shifted out. MLT1 SLA (IX+8) RL (IX+9) RL (IX+10) RL (IX+11) RL (IX) RL (IX+1) RL $(IX+2)$ RL (IX+3) JR NC, MLT2 LD $A, (IX+8)$ ADD $A, (IX+4)$ LD $(IX+8)$, A LD $A, (IX+9)$ ADC A , (IX+5) LD $(IX+9)$, A LD A,(IX+10) ADC $A, (IX+6)$ LD $(IX+10)$, A $LD \qquad A, (IX+11)$ ADC A , (IX+7)

 LD (IX+11),A JR NC, MLT2 INC (IX)
JR NZ.M NZ, MLT2 INC (IX+1) JR NZ, MLT2 INC $(IX+2)$ JR NZ, MLT2 INC (IX+3) MLT2 DJNZ MLT1 ; Store bytes 4-7 in Mltbuf 8-15. $LD \tA, (IX)$ LD (IX+12),A LD $A, (IX+1)$ LD $(IX+13)$, A $LD \qquad A, (IX+2)$ LD $(IX+14)$, A LD $A, (IX+3)$ LD $(IX+15)$, A RET Routine: Mult Function: Multiply two floating point numbers Called by: Divide, Input, Meas, Print, Read, Visc Calls: Mlt, Norm, Regld, Regsv Entry: BC points to #1, DE points to #2, HL points to result Exit: Result stored at HL Preserved: All MULT CALL REGSV PUSH HL PUSH BC
LD TX IX, MLTBUF CALL MULT7 ; Move number 2 to mltbuf. LD A , (DE) LD (MULTE),A ; Exponents are held in Multe. POP DE
CALL MU MULT7 ; Move number 1 to Mltbuf+4. LD $A, (DE)$ LD B,A LD A, (MULTE) ADD A,B ; Add the exponents. LD (MULTE),A LD A,(MLTBUF+3) BIT 7,A JR NZ, MULT1 ; Check the sign of number2: the B register is set to 0 if positive, 255 if negative. LD $B, 0$ SET 7, A LD (MLTBUF+3),A JR MULT2 MULT1 LD B,255 MULT2 LD A, (MLTBUF+7) BIT 7,A JR NZ, MULT3 SET 7, A

 LD (MLTBUF+7),A ; Check the sign of number 1, if it is positive then the result sign is that of number two, otherwise invert the sign. The sign is held in Mltsgn. LD A,B JR MULT4 MULT3 LD A,B CPL. MULT4 LD (MLTSGN),A ; 32 bit multiplication is performed by Mlt, and the result normalised by calling subroutine Norm. CALL MULT CALL NORM LD A,(MLTSGN) OR A JR NZ, MULT5 RES 7,(IX+15) ; Insert the sign bit into the result. MULT5 POP HL LD IX,MLTBUF+12 LD B, 4 ; Move the result to the location pointed to by HL. MULT6 LD A,(IX) LD (HL),A INC HL INC IX DJNZ MULT6 LD A,(MULTE) ; Store exponent byte also. LD (HL),A CALL REGLD RET MULT7 LD B,4 ; Subroutine Mult7 is used to transfer the two numbers into space at Mltbuf. MULT8 LD A,(DE) LD (IX),A INC DE INC IX DJNZ MULT8 LD A,(DE) RET Routine: Norm Function: Normalise a floating point number Called by: Add, Mult, Recip Calls: None Entry: 64-bit number is from IX+8 to IX+15 Exit: 64-bit number is from IX+8 to IX+15, Multe is adjusted as necessary Preserved: C, D, E, H, L, IX, IY NORM LD B, 32 NORM1 LD A,(IX+15) ; Normalise by shifting left and decrementing the exponent until a 1 appears in the Most Significant Place. BIT 7,A RET NZ SLA $(IX+8)$ RL (IX+9) RL (IX+10) RL (IX+11) RL (IX+12)

 RL (IX+13) RL (IX+14) RL (IX+15) LD A,(MULTE) DEC A LD (MULTE),A DJNZ NORM1 RET Routine: Pb2 Function: Program B2: Continuous viscosity measurement Called by: Main Calls: Meas, Print, Vischk, Wait Entry: None Exit: As from Wait Preserved: None PB2 LD HL, VISCTY ; Measure, Check it falls within the set range, print, and wait for a keypress. CALL MEAS CALL PRINT CALL VISCHK JR Z, PB2 LD HL, VISCTY CALL PRINT CALL WAIT RET Routine: Pb3 Function: Program B3: Timed measurements Called by: Main, Pb4 Calls: Alarm, Alm2, Equals, Keyb, Meas, Print, Vischk. Entry: None Exit: None Preserved: None PB3 CALL ALM2 ; Set the next alarm time. LD HL, LOG LD (LOGCUR),HL ; Initialise the result pointers to the start of the result area, and set measurement number zero. LD HL,0 LD (LOGN),HL LD IX,CLKFLG SET 7, IX ; Display the clock, and jump to the first measurement. JR PB3D PB3A CALL KEYB ; Ckeck the keyboard; if ´B' pressed, display the time, if 'A' pressed, display the last viscosity measured. LD IX,CLKFLG CP 11 JR NZ, PB3B
SET 7, (IX) $7,(\text{IX})$ JR PB3C PB3B CP 10 JR NZ, PB3C
RES 7, (IX) $7, (IX)$

 LD HL,VISCTY ; Display last viscosity. CALL PRINT PB3C CALL ALARM ; Check to see if alarm period has expired yet. If so, take a reading. JR NZ,PB3A PB3D LD HL, VISCTY CALL MEAS ; Measure and print the viscosity, and store it at the current result location. CALL PRINT LD DE,(LOGCUR) CALL EQUALS LD HL,(LOGCUR) ; Increment the result pointer. INC HL INC HL INC HL INC HL INC HL LD (LOGCUR),HL LD BC,(LOGNMX) LD DE,(LOGN) INC DE LD (LOGN),DE ; Increment the result number, and check that it does not equal the number of results requested by the user. LD A,C CP E JR NZ,PB3E LD A,B CP D ; Return if all measurements are done. RET Z PB3E CALL VISCHK ; Check that the viscosity is within the user defined range, and return if not. JR Z, PB3A RET Routine: Pb4 Function: Program B4: As Pb3 except program B4 displays time elapsed since start of experiment, not real-time Called by: Main Calls: Pb3 Entry: None Exit: None Preserved: None PB4 LD IX,CLKSEC XOR A LD B, 6 ; Set all time bytes to zero and reset the 50 Hz counter, then jump to Pb3. PB4A LD (IX), A TNC TX DJNZ PB4A IN A , (6) LD (CLK50),A JP PB3 Routine: Pc Function: Program C: Scan through the measurements

Called by: Main Calls: Intfp, Keyb, print Entry: None Exit: None Preserved: None PC LD HL, 0 ; Initialise the result pointer and the result number. LD (LOGN),HL LD HL,LOG LD (LOGCUR),HL XOR A LD (LOGFLG),A ; Logflg holds the display format: if 0, the measurement number is displayed, if 1, the measured viscosity is displayed. PCA LD A,(LOGFLG) OR A JR NZ,PCB LD HL,(LOGN) ; Convert measurement number to floating point format, and display. LD IX, NUM1 CALL INTFP LD HL,NUM1 CALL PRINT JR PCC PCB LD HL,(LOGCUR) ; Print measured viscosity. CALL PRINT PCC CALL KEYB CP 19 ; Return from Program C if Clr key is pressed. RET Z CP 10 JR NZ,PCD ; If 'A' pressed, enter display format 0. XOR A LD (LOGFLG),A JR PCA PCD CP 11 JR NZ,PCE ; If 'B' pressed, enter display format 1. LD (LOGFLG),A JR PCA PCE CP 20 ; If '+' pressed, then increment the result pointer to the next result, and increment the result number. JR NZ, PCF
LD HL, (LO HL,(LOGCUR)
HL INC INC HL INC HL INC HL INC HL LD (LOGCUR),HL LD HL,(LOGN) INC HL LD (LOGN),HL LD DE,(LOGNMX) ; Check that the result number is not more than the number of results there are, and restart Pc if it is. LD A,L CP E JR NZ,PCA

 LD A,H CP D JR NZ,PCA JR PC PCF CP 18 ; If '-' key pressed, then decrement the result pointer to the next result, and decrement the result number. JR NZ,PCC LD HL,(LOGCUR) DEC HL DEC HL DEC HL DEC HL DEC HL LD (LOGCUR),HL LD HL,(LOGN) DEC HL LD (LOGN),HL LD A,255 CP H ; Check that the result number is not now negative, and restart Pc if it is. JR NZ,PCA JP Z,PC Routine: Print Function: Displays a floating point number Called by: Calib, Main, Pb2, Pb3, Pc Calls: Err, Mlt, Mult, Regld, Regsv Entry: HL points to the number Exit: Error 1: Print overflow, Error 2: Print negative attempted Preserved: All PRINT CALL REGSV XOR A LD (PRIOVR),A LD (PRIEXP),A ; Priovr is a flag indicating print overflow, Priexp holds the decimal exponent of the number, Pribuf is a 7 byte temporary storage space. LD BC,5 LD DE,PRIBUF LDIR ; Transfer the number into Pribuf. LD IY,PRIEXP LD A,(PRIBUF+3) RL A ; Check the number is positive, if not jump to Prin21, to signal error 2. JP C,PRIN21 LD A,(PRIBUF+4) CP 128 ; Investigate size of the number: if less than 1, call Prin15; if greater than 1, call Prin14. These routines reduce the magnitude of the binary exponent. CALL C,PRIN14 CALL NC,PRIN15 LD IX,PRIBUF SET $7, (IX+3)$ OR A JR Z, PRIN2 LD B,A ; Multiply by two by shifting right, until the binary exponent becomes zero. This completes the binary to decimal conversion. PRIN1 SRL (IX+3)

 RR (IX+2) RR (IX+1) RR (IX) DJNZ PRIN1
PRIN2 LD IX.ML LD IX, MLTBUF LD HL,PRIBUF LD BC, 4 LD DE,MLTBUF LDIR ; Move the number to mltbuf. LD B, 7 LD IY,PRIBUF ; The next part converts the binary fraction to decimal by repeatedly multiplying by ten and taking the integer part, until seven decimal digits have been built up in Pribuf. PRIN3 LD A,10 LD $(IX+4)$, A XOR A LD $(IX+5)$, A LD $(IX+6)$, A LD $(IX+7)$, A ; Put 10 in Mltbuf 4-7 PUSH BC CALL MLT POP BC $LD \tA, (IX+12)$ LD (IY),A ; Store integer part in Pribuf and move the result back into Mltbuf 0-3. INC IY LD HL,(MLTBUF+8) LD (MLTBUF),HL LD HL,(MLTBUF+10) LD (MLTBUF+2), HL DJNZ PRIN3 LD A,(PRIEXP) DEC A CP 127 ; Investigate the decimal exponent; if the number is less than 1, call Prin9, if greater than 1, continue at Prin4. JR C, PRIN4 CALL PRIN9 LD A,(PRIOVR) OR A JR Z, PRIN5 ; If the number is less than 0.00001, then just print '0.' and return, otherwise jump to prin5. LD A,17 OUT (8),A LD A,32 OUT (144),A JR PRINZ PRIN4 CP 6 ; If the decimal exponent is too big to display then jump to Prin17 to indicate error 1. NC, PRIN17 CALL PRIN18 LD A,(PRIOVR) OR A ; Jump to Prin17 in the event of an overflow. JP NZ,PRIN17 PRIN5 LD A,255 PUSH AF ; Next shift out all the leading zeros, using the A register to hold the information to be sent to the digit blanking register, Out 144.

PRIN6 LD A,(PRIBUF+5) OR A JR NZ, PRIN7
LD BC, 5 LD BC, 5
LD HL, P HL, PRIBUF+4 LD DE,PRIBUF+5 LDDR POP AF
SLA A SLA PUSH AF
JR PRING JR PRIN PRIN7 LD B, 6 LD C,13 LD HL,PRIBUF ; Output the contents of Pribuf to the displays, and set the digit blanking register, Out 144, appropriately. PRIN8 LD A,(HL) OUT (C),A DEC C INC HL DJNZ PRIN8 POP AF OUT (144),A ; Jump to the routine end. JR PRINZ PRIN9 LD IX,PRIBUF+5 ; First round the number by checking the least significant digit, and if greater than or equal to 5, incrementing the last digit of the displayed number. LD $A, (IX+1)$ CP 5 JR C,PRIN11 PRIN10 LD A,(IX) INC A LD (IX) , A
CP 10 CP 10 JR NZ, PRIN11 XOR A LD (IX), A
DEC IX DEC JR PRIN10 PRIN11 LD HL,PRIBUF LD A,(PRIEXP) DEC A ; Create appropriate leading zeros by shifting the number right, until the exponent becomes zero. PRIN12 OR A JR Z, PRIN13 LD BC, 5
LD HL, P HL, PRIBUF+4 LD DE,PRIBUF+5 LDDR PUSH AF XOR A LD (PRIBUF),A POP AF INC A
JR PF PRTN12 PRIN13 LD A,(PRIBUF) ; Insert a decimal point after the leftermost zero, then return. OR 16 LD (PRIBUF),A RET PRIN14 LD A,(PRIBUF+4) ; Multiply the number by a tenth until it is less than one, i.e the integer part

is reduced to zero; for each multiplication increment the decimal exponent. LD B,A XOR A
SUB B SUB B
CP 4 CP RET C LD BC,TENTH LD DE,PRIBUF LD HL,PRIBUF CALL MULT INC (IY)
JR PRIN PRIN14 PRIN15 LD A,(PRIBUF+4) ; Multiply the number by ten until any futher multiplications would make it greater than one; for each multiplication, decrement the decimal exponent. CP 252 JR C, PRIN16 LD B,A XOR A SUB B RET PRIN16 LD BC, TEN LD DE,PRIBUF LD HL,PRIBUF CALL MULT DEC (IY) JR PRIN15 PRIN17 LD A, 1 ; Signal print overflow error. CALL ERR JR PRINZ ; Subroutine Prin18 rounds the number, by checking the least significant digit and if greater than or equal to 5, incrementing the last digit of the displayed number.
PRIN18 LD IX, PRIBUF+5 LD $A, (IX+1)$ CP 5 JR C,PRIN20 PRIN19 LD A, (IX) INC A LD (IX),A CP 10 JR NZ, PRIN20 ; If incrementing the last digit resulted in a number > 10, it must be reset and the next digit incremented, and so on until no more overflows occur, XOR A LD (IX),A DEC IX JR PRIN19
LD HL, PRIBUF PRIN20 LD LD A,(PRIEXP) DEC A ; Calculate position of the decimal point in the print buffer and inser it by Or 16. LD E, A
T.D D.O LD D, 0
ADD HI_L HL, DE LD A,16 OR (HL) LD (HL),A RET PRIN21 LD A, 2 ; Signal print negative error. CALL ERR

 RET Routine: Range Function: Finds minimum and maximum motor speeds that are suitable for the set of measurements Called by: Visc Calls: Chk1, Chk2, Chk3, Divide, Intfp, Sub
Entry: None Entry: Exit: Mtrmin, Mtrmax set; C flag is set on error Preserved: None RANGE CALL CHK1 ; Find the maximum motor speed, angle < 170 degrees; return on error. RET C
CALL CHK2 CALL ; Find minimum motor speed, angle >0. CALL CHK3 ; Check max speed is more than min speed, return on error. RET C LD A,(MTRMIN) LD L,0 LD H,0 LD IX,RNGMAX ; Convert max speed to floating point. CALL INTFP LD A,(MTRMAX) LD L,0 LD H,A LD IX,RNGMIN ; Convert min speed to floating point. CALL INTFP LD BC, RNGMAX LD DE, RNGMIN LD HL,RNG ; Calculate range. CALL SUB LD BC,RNG LD DE,TEN LD HL, RNGINC ; Calculate motor speed increment. CALL DIVIDE OR A RET Routine: Read Function: Reads mechanism: displacement angle and motor speed. Called by: Chk1, Chk2, Visc Calls: Add, Clock, Divide, Mark, Mult, Recip, Regld, Regsv, Space Entry: DE points to angle, HL to speed Exit: Angle, speed stored at DE, HL respectively. NC flag set on error Preserved: None

PRINZ CALL REGLD ; Terminate Print routine.

; Initialise variable Timerb: Read6 is used to see that if no change in mechanism state happens within 2 seconds, the program jumps to Readfl, and returns from this routine with the NC flag set. Normal termination is with the C flag set.
READ2 C CALL READ6 JP NC,READFL IN A,(14) RL A ; Read in mechanism state, and repeat until it becomes 0. JR C,READ2 IN A , (6) LD (TIMERB),A READ3 CALL READ6 JR NC, READFL IN A,(14) RL A ; Read in mechanism state and repeat until it becomes 1. JR NC, READ3 DJNZ READ1 IN A , (7) LD HL,NUM1 IN A , (6) LD (TIMERB),A READ4 CALL READ6 JR NC,READFL IN A,(14) RL A ; Read in mechansim state and repeat until it becomes 0. JR C, READ4 ; Now call subroutine Space, to read in the space period. CALL SPACE LD HL,NUM2 IN $A_{1}(6)$ LD (TIMERB),A READ5 CALL READ6 JR NC, READFL IN A,(14) RL A ; Read in mechanism state and repeat until it becomes 1. JR NC, READ5 ; Now call subroutine Mark, to read in the mark period. CALL MARK LD BC,NUM1 LD DE,NUM2 LD HL,NUM3 ; Add mark and space periods to get the total rotation period. Next take the reciprocal to get the motor speed. CALL ADD LD DE,NUM3 POP HL CALL RECIP LD BC,NUM2 LD DE,NUM3 LD HL,NUM4 ; Divide Mark by the total period and multiply by 360 degrees, to get the displacement angle. CALL DIVIDE LD BC,THRE60 LD DE,NUM4 POP HL CALL MULT SCF RET READ6 CALL REGSV

; Update clock. CALL CLOCK CALL REGLD LD A,(TIMERB) LD D,A IN $A_{1}(6)$ SUB D JP P, READ7 NEG ; Check that 2 seconds have not passed. READ7 CP 100 RET READFL POP HL ; On error restore stack and return. POP HL RET Routine: Recip Function: Calculates the reciprocal of a floating point number Called by: Divide, Read Calls: Error, Norm, Regld, Regsv Entry: DE points to the number, HL to the result Exit: Result stored at HL; unchanged on error Preserved: All RECIP CALL REGSV PUSH HL LD HL,MLTBUF LD B,16 XOR A ; Clear Mltsgn, used to hold the sign, and clear Mltbuf, used as temporary space. LD (MLTSGN),A RCP1 LD (HL), A INC HL INC DJNZ RCP1 LD L,E LD H,D LD DE,MLTBUF+4 LD BC, 4 LDIR ; Transfer the number into Mltbuf+4. LD A,(HL) POP HL NEG CP 128 ; Jump to Rcperr to signal error, on division by floating point zero. JP Z,RCPERR PUSH HL INC A ; Multe holds the exponent part. LD (MULTE),A LD IX,MLTBUF BIT $7, (IX+7)$ JR Z, RCP2 LD A,1 ; Check the sign and store it in Mltsgn. LD (MLTSGN),A RCP2 SET $7, (IX+7)$; Mltbuf 0-7 holds the number, Mltbuf 8-11 holds the result, Mltbuf 12-15 holds the remainder, initially set to 1.

SET 7, (IX+15) ; Initially rotate the number right 1 bit, so that the first subtraction does not automatically result in a negative remainder. SRL (IX+7) RR (IX+6) RR (IX+5) RR $(IX+4)$ RR (IX+3) RR (IX+2) RR (IX+1) RR (IX) LD B,32 ; Use the B register as a bit counter: the loop must be run 32 times. JR RCP4 RCP3 SLA (IX+8) ; Shift the result and remainder left by one bit. RL (IX+9) RL (IX+10) RL (IX+11) RL (IX+12) RL (IX+13) RL (IX+14) RL (IX+15) RCP4 LD HL, (MLTBUF+12) LD DE,(MLTBUF+4) ; Here subtract the number from the remainder. SBC HL,DE LD (MLTBUF+12), HL LD HL,(MLTBUF+14) LD DE,(MLTBUF+6) SBC HL,DE LD (MLTBUF+14), HL JR C,RCP5 ; If the result is still positive, insert a '1' into the result and loop; otherwise jump to Rcp5. INC $(IX+8)$ JR RCP6 RCP5 LD HL, (MLTBUF+12) ; The number is added back to the remainder to make it positive again, and a 0^o is automatically inserted into the result by doing nothing and just waiting for a '0' to be shifted in in the next pass through the loop. LD DE,(MLTBUF+4) ADD HL,DE LD (MLTBUF+12), HL ÖD HL,(MLTBUF+14) LD DE,(MLTBUF+6) ADC HL,DE LD (MLTBUF+14), HL
RCP6 DJNZ RCP3 DJNZ RCP3 LD IX,MLTBUF-4 ; Call subroutine Norm to normalise the result. CALL NORM LD IX,MLTBUF+8 RES $7, (IX+3)$
I.D $A, (MLTSG)$ A, (MLTSGN) OR A ; Jump if positive, otherwise restore the sign bit to a '1'. JR Z, RCP7 SET $7, (IX+3)$ RCP7 POP HL LD B, 4 ; Move the result to the the address pointed to by HL. RCP8 LD A, (IX) LD (HL),A
INC HL INC IX DJNZ RCP8 ; Store the exponent part too. LD A,(MULTE) LD (HL), A
JR RCPZ RCPZ RCPERR XOR A CALL ERROR ; Restore registers and return. RCPZ CALL REGLD RET Routine: Regld Function: Loads all the registers off the stack Called by: Almvis, Calib, Divide, Err, Input, Meas, Mult, Print, Read, Recip, Sub, Visc Calls: None Entry: None Exit: All Preserved: None REGLD POP IX POP HL POP DE POP BC POP AF POP IY EX (SP), IX ; Restore subroutine return address. RET Routine: Regsv Function: Saves all the registers to the stack Called by: Almvis, Calib, Divide, Err, Input, Meas, Mult, Print, Read, Recip, Sub, Visc. Calls: None Entry: All Exit: All Preserved: All REGSV EX (SP), IX PUSH IY PUSH AF PUSH BC PUSH DE PUSH HL PUSH IX ; Restore subroutine return address. RET outine: Reset Function: Restarts the entire system, if RST is pressed for longer than 0.5s Called by: Clock.
Calls: None Calls: Entry: None Exit: None

Preserved: C, D, E, H, L, IX, IY RESET IN A, (8) OR 224 CP 239 ; Check if Rst key is being pressed, return if not. RET NZ IN A , (6) ADD A,25 ; Load B with current 50 Hz counter value + 25. LD B,A RESET1 IN A, (8) OR 224 CP 239 ; Check that the Rst key is still pressed. RET NZ IN A , (6) CP B ; Loop until 0.5 seconds have passed. JR NZ, RESET1 ; Jump to 0, i.e a system reset. RST 0 Routine: Space Function: Counts "Space" of mark/space ratio Called by: Read Calls: None Entry: HL point to the location Space will be stored at Exit: Space stored at HL Preserved: None SPACE IN $A_{1}(0)$ LD E,A IN $A_{1}(1)$ LD D,A IN A , (2) LD C,A ; Read ports 0-2 into E,D,C registers. LD B.24 XOR A SPACE1 BIT 7, C ; Test the leftermost bit and jump if its a '1', otherwise normalise by shifting one bit to the left, and repeating. JR NZ, SPACE2 SLA E RL D RL C DEC A ; Reduce the exponent, held in A. DJNZ SPACE1 SPACE2 RES 7, C Store the result at HL. LD (HL), 0 INC HL LD (HL), E INC HL LD (HL),D INC HL LD (HL),C INC HL

Routine: Sub Function: Subtracts two floating point numbers Called by: Chk1, Range, Visc, Vischk. Calls: Add, Regld, Regsv Entry: BC points to #1, DE to #2, HL to result #1-#2 Exit: Result stored at HL Preserved: All SUB CALL REGSV LD BC,5 LD L,E LD H,D LD DE,PRIBUF LDIR ; Transfer the second number into temporary storage space at Pribuf. LD IX,PRIBUF RL $(IX+3)$ **CCF** ; Invert the sign bit of the second number's copy at Pribuf. RR $(IX+3)$ CALL REGLD PUSH DE LD DE,PRIBUF ; Call subroutine add; inverting the second number's sign bit makes this addition effectively the required subtraction. CALL ADD POP DE RET Routine: Visc Function: Reads the absolute, uncalibrated viscosity, does a least squares best fit on the data Called by: Calib, meas Calls: Add, Divide, Equals, Fpint, Mult, Range, Read, Regld, Regsv, Sub Entry: HL points to address of viscosity variable Exit: C flag is set on error; viscosity is stored at HL Preserved: All VISC CALL REGSV PUSH HL ; Set the statistical variables initially equal to zero. LD DE,STATXX LD HL,ZERO CALL EQUALS LD DE,STATXY CALL EQUALS LD DE,STATYY CALL EQUALS LD DE,STATX CALL EQUALS LD DE,STATY CALL EQUALS CALL RANGE ; Call subroutine Range to find the range of measurement. RET C

XOR A

LD (HL),A

RET

 OUT (143),A LD DE,NUM6 LD HL, NUM7 LD B,10 ; Call read with ten revolutions at maximum speed. CALL READ LD B,10 ; Use B as an index variable, to count the 10 readings. VISC1 PUSH BC LD IX,RNGMIN Convert Rngmin to integer and output this motor speed to the DAC. CALL FPINT LD A,L OUT (142),A LD A,H OUT (143),A LD DE,NUM6 LD HL,NUM7 LD B,10 ; Take the reading, with 10 revolutions. CALL READ ; Now compute the various statistical variables that are required for the best fit. See text for explanation. LD BC,NUM7 LD DE,NUM7 LD HL,NUM8 CALL MULT LD BC,STATXX LD DE,NUM8 LD HL,STATXX CALL ADD LD BC,NUM7 LD DE,NUM6 LD HL,NUM8 CALL MULT LD BC,STATXY LD DE,NUM8 LD HL, STATXY
CALL ADD $CALL$ LD BC,NUM6 LD DE,NUM6 LD HL,NUM8 CALL MULT LD BC,STATYY ÖD DE,NUM8 LD HL,STATYY CALL ADD LD BC,NUM7 LD DE,STATX LD HL,STATX CALL ADD LD BC,NUM6 LD DE,STATY LD HL,STATY CALL ADD LD BC,RNGMIN LD DE,RNGINC LD HL, RNGMIN ; Add the range increment to Rngmin to get the new motor speed. CALL ADD POP BC ; Loop if 10 readings have not yet been taken. DJNZ VISC2 JR VISC3

 PUSH HL POP IX BIT 7, (IX+3) JR Z, VISCH1 JR Z, V
LD A, 8 CALL ERROR INC A ; Inc A to reset the Z flag, signifying that an error occurred. RET VISCH1 LD BC, VISMAX
LD DE, VISCTY LD DE, VISCTY
LD HL, NUM1 HL,NUM1
SUB $CALL$; Subtract Vismax from the viscosity, and signal error 9 if the result is negative. BIT 7,(IX+3) RET Z $LD \tA, 9$ CALL ERROR INC A ; Inc A to reset the Z flag, signifying that an error occurred. RET Routine: Wait Function: Waits for a keypress Called by: Error, Main, Pb2
Calls: Keyb Calls: Entry: None Exit: A holds keycode Preserved: E, IX, IY WAIT CALL KEYB ; Scan keyboard, and loop if no key was pressed. CP 255 JR Z, WAIT RET

APPENDIX C: Engineering Drawings

1: dépieral doing; made dessertés Branchenferster des des ca Outside screese to E, Mide end acrees to F $J:$ Glass rods to be inserted will have a more dian of 32mm, 10 ID g'G" is 3.3 mm. K: 4 off : Correr pillars from Ø6mm ontiⁿ rod, length 32mm,

APPENDIX D: Numerical Results

APPENDIX D1: 4.1.3: Angular disulacement and motor speed

(Results are shown to all available decimal places regardless of significance)

300 cst fluid:

1000 cst fluid:

10000 cst fluid:

APPENDIX D2: 4.2 Dependence of Viscosity on Temperature.

1000 cst DC200 lubricant

10000 cst DC200 lubricant

APPENDIX D3: 4.3 Accuracy and long term stability

Carried out at room temperature on 1000 cst DC200 lubricant. 128 readings, every half hour for 64 hours.

Viscosity readings:

949.558 1001.91 946.369 958.979 877.139 1002.74 974.926 962.344 947.033 1001.93 978.834 976.368 1001.61 869.818 971.86 906.964 949.041 907.625 995.89 996.089 1007.34 934.708 960.586 977.113 977.58 979.538 971.364 965.091 976.265 988.612 985.19 954.478 943.996 967.377 898.123 959.248 960.554 950.565 935.06 930.973 947.318 951.726 977.987 958.262 941.756 921.744 916.805 937.076 1018.84 940.871 846.857 905.924 939.983 916.391 941.499 976.613 971.107 930.231 941.97 965.632 989.284 999.076 991.629 945.657 957.833 912.483 969.333 981.724 925.521 969.501 923.887 962.41

964.472 962.098 878.744 881.49 1008.05 953.882 912.241 909.709 915.393 989.029 1000.47 901.13 969.148 842.929 934.306 863.771 930.226 995.574 998.382 889.828 966.483 973.489 991.375 900.589 1013.52 896.325 913.582 927.039 999.756 955.862 971.057 940.237 1044.38 955.391 910.862 931.014 933.844 919.38 911.379 880.704 962.224 922.067 901.848 923.138 916.182 930.647 942.24 950.281 929.404 927.812 946.464 879.78 945.831 925.414 917.934 933.968